Master in Space Science and Technology

Thermal engineering





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Thermal engineering

Thermodynamics

- Basics
 - Energy and entropy
 - Temperature and thermometry
 - Variables: state properties, process functions
 - Equations of state, simple processes
 - Phase change
- Applied:
 - Mixtures. Humid air (air conditioning)
 - Thermochemistry (combustion)
 - Heat engines (power generation)
 - Refrigeration (cold generation)
 - Thermal effects on materials and processes
 - Thermofluiddynamic flow 1D...

Heat transfer (conduction, convection, radiation, heat exchangers)



Thermodynamics

Basic thermodynamics

- The science of heat and temperature. Work. Energy. Thermal energy.
- Energy and entropy. The isolated system. The traditional Principles
- Generalisation (mass, momentum, energy): the science of assets (conservatives do not disappear) and spreads (conservatives tend to disperse)
- Type of thermodynamic systems (system, frontier, and surroundings)
 - Isolated system: $\Delta m=0$, $\Delta E=0$
 - Closed system : $\Delta m=0$, $\Delta E\neq 0$
 - Open system : $\Delta m \neq 0$, $\Delta E \neq 0$
 - Type of thermodynamic variables
 - Intensive or extensive variables
 - State or process variables
- Type of thermodynamic equations
 - Balance equations (conservation laws); e.g. ∆E_{close-sys}=W+Q
 - Equations of state (constitutive laws); e.g. pV=mRT
 - Equilibrium laws: $S(U, V, n_i)_{iso-sys}(t) \rightarrow S_{max} e.g. dS/dU|_{V,ni}$ =uniform...
 - (Kinetics is beyond classical thermodynamics; e.g. $\vec{q} = -k\nabla T$)
- Applied thermodynamics

Thermodynamics (cont.)

• Basic thermodynamics

Applied thermodynamics

- Energy and exergy analysis (minimum expense and maximum benefit)
- Non-reactive mixtures (properties of real mixtures, ideal mixture model...)
- Hygrometry (humid air applications: drying, humidification, air conditioning...)
- Phase transition in mixtures (liquid-vapour equilibrium, solutions...)
- Reactive mixtures. Thermochemistry. Combustion
- Heat engines
 - Gas cycles for reciprocating and rotodynamic engines
 - Vapour cycles (steam and organic fluid power plants)
- Refrigeration, and heat pumps
 - Cryogenics (cryocoolers, cryostats, cryopreservation...)
- Thermal analysis of materials (fixed points, calorimetry, dilatometry...)
- Non-equilibrium thermodynamics (thermoelectricity, dissipative structures...)
- Environmental thermodynamics (ocean and atmospheric processes...)



Balance equations

Magnitude	<u>Accumul</u>		Production	Impermeable flu	ux Permeable flux
mass	d <i>m</i>	=	0	+0	$+\Sigma dm_e$
momentum	$d(m \vec{v})$	=	$m\vec{g}$ dt	$+\vec{F}_A$ dt	$+\Sigma \vec{v}_e \mathrm{d}m_e - \Sigma p_e A_e \vec{n}_e \mathrm{d}t$
energy	d(<i>me</i>)	=	0	+dW+dQ	$+\Sigma h_{\rm te} {\rm d} m_{\rm e}$
entropy	d(<i>ms</i>)	=	dS _{gen}	+dQ/T	$+\Sigma_{S_{e}} dm_{e}$
exergy	d(<i>m ø</i>)	=	$-T_0 dS_{gen}$	$+ dW_{u} + (1 - T_0/T) dQ$	$2 + \Sigma \psi_{\rm e} dm_{\rm e}$

with
$$e=u+e_{m}=u+gz+v^{2}/2$$

 $dW=\int_{IF}Fdx=\int_{IF}Md\theta, \quad W_{u}=W+p_{0}\Delta V$
 $h=u+pv, \quad h_{t}=h+e_{m}$
 $ds=(du+pdv)/T=(dq+de_{mdf})/T, \quad de_{mdf}\geq 0, \quad dS_{gen}\geq 0$
 $\phi=e+p_{0}v-T_{0}s, \quad \psi=h_{t}-T_{0}s$

Substance data

Perfect gas model

- Ideal gas: pV=mRT or $pV=nR_uT$ ($R=R_u/M$, $R_u=8.3$ J/(mol·K))
- Energetically linear in temperature: $\Delta U = mc_v \Delta T$
- <u>Air data</u>: R=287 J/(kg·K) and $c_p = c_v + R = 1000$ J/(kg·K), or M=0.029 kg/mol and $\gamma = c_p/c_v = 1.4$

Perfect solid or liquid model

- Incompressible, undilatable substance: V=constant (but beware of dilatations!)
- Energetically linear in temperature: $\Delta U = mc \Delta T$
- <u>Water data</u>: ρ=1000 kg/m³, c=4200 J(kg·K)

Perfect mixture (homogeneous)

- Ideal mixture $v = \sum x_i v_i^*$, $u = \sum x_i u_i^*$, $s = \sum x_i s_i^* R \sum x_i \ln x_i$
- Energetically linear in temperature: $\Delta U=mc_v\Delta T$

Heterogeneous systems

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- Phase equilibria of pure substances (Clapeyron's equation)
- Ideal liquid-vapour mixtures (Raoult's law): $\frac{x_{v_1}}{r_1} = \frac{p_1^*(T)}{r_1}$
- Ideal liquid-gas solutions (Henry's law): $\frac{c_{L,s}}{c} = K_{s,cc}^{dis}(T)^{x_{L1}}$

Real gases. The corresponding state model, and other equations of state.

 $\frac{dp}{dT} = \frac{\Delta h}{T \Delta v}$

Thermodynamic processes

V=cte.

p = cte.

 $\eta_{C} \equiv \frac{w_{s}}{w} = \frac{h_{2ts} - h_{1t}}{h_{2t} - h_{1t}} \stackrel{\text{PGM}}{=} \frac{\left(p_{2t}/p_{1t}\right)^{\frac{r}{\gamma}} - 1}{T_{2t}/T_{1t} - 1} \quad \eta_{T} \equiv \frac{w}{w_{s}} \stackrel{\text{PGM}}{=} \frac{1 - T_{1t}/T_{2t}}{1 - \left(p_{s}/p_{s}\right)^{\frac{\gamma-1}{\gamma}}}$ - Open system: $w = \Delta h = c_p(T_2 - T_1)$ Internal energy equation (heating and cooling processes) $\Delta U \equiv \Delta E - \Delta E_m = Q + E_{mdf} - \int p dV$ One-dimensional flow at steady state $\dot{m}_{in} = \dot{m}_{out} = \rho v A = \rho \dot{V}$ $\Delta h = w + q$ $w = \int \frac{dp}{dr} + \Delta e_m + e_{mdf}$ Thermodynamic processes in engines • $\begin{array}{c|c} \text{Electrical} \\ \text{Engine} \end{array} \rightarrow W & \mathcal{Q}_1 \rightarrow \\ \hline \text{Heat} \\ \text{Engine} \end{array} \rightarrow W & m_f \rightarrow \\ \hline \text{Chemical} \\ \text{Engine} \\ \hline \text{Regine} \end{array}$ Reference Atmosphere Reference Atmosphere Reference Atmosphere Carnot cycle Otto cycle

Adiabatic non-dissipative process of a perfect gas:

Fluid heating or cooling

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At constant volume: $Q=\Delta U$

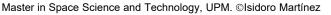
- At constant pressure: $Q = \Delta H = \Delta (U + pV)$

Close system: $w = \Delta u = c_v (T_2 - T_1)$

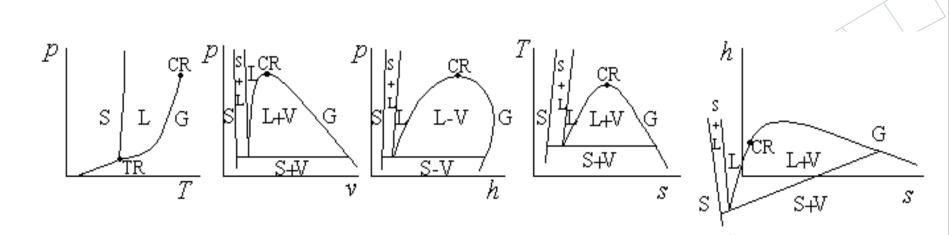
Adiabatic gas compression or expansion

 $dE = dQ + dW \rightarrow dU = -pdV \rightarrow mc_v dT = -\frac{mRT}{V}dV$

 $\rightarrow \frac{dT}{T} + \frac{R}{c} \frac{dV}{V} = 0 \quad \rightarrow \quad Tv^{\gamma-1} = \text{cte.}, \ pv^{\gamma} = \text{cte.}, \ T/p^{\frac{\gamma-1}{\gamma}} = \text{cte.}$



Phase diagrams (pure substance)

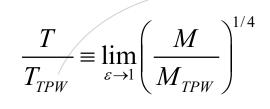


- Normal freezing and boiling points (p₀=100 kPa)
- Triple point (for water T_{TR}=273.16 K, p_{TR}=611 Pa)
- Critical point (for water T_{CR}=647.3 K, p_{TR}=22.1 MPa)
- Clapeyron's equation (for water h_{sL}=334 kJ/kg, h_{LV}=2260 kJ/kg)

$$\frac{dp}{dT}\Big|_{sat} = \frac{h_V - h_L}{T(v_V - v_L)} \xrightarrow{v_V > v_L, v_V = RT/p, h_{LV} = const} \ln\left(\frac{p}{p_0}\right) = \frac{-h_{LV}}{R}\left(\frac{1}{T} - \frac{1}{T_0}\right)$$

Thermometry

- Temperature, the thermal level of a system, can be measured by different primary means:
 - The ideal-gas, constant-volume thermometer
 - The acoustic gas thermometer
 - The spectral radiation thermometer
 - The total radiation thermometer
 - The electronic noise thermometer

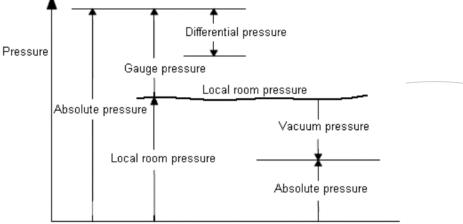


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- The temperature unit is chosen such that $T_{\text{TPW}} = 273.16 \text{ K}$
- The Celsius scale is defined by $T/^{\circ}C = T/K-273.15$
- Practical thermometers:
 - Thermoresistances (e.g. Pt100, NTC)
 - Thermocouples (K,J...).

Piezometry

- Pressure (normal surface force per unit normal area), is a scalar magnitude measured by difference (in non-isolated systems; recall free-body force diagrams).
- Gauge and absolute pressure:



- Pressure unit (SI) is the pascal, 1 Pa=1 N/m² (1 bar=100 kPa)
- Hydrostatic equation:

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$$\frac{dp}{dz} = -\rho g \quad \rightarrow \quad \begin{cases} \xrightarrow{PLM} & p = p_0 - \rho g \left(z - z_0 \right) \\ \xrightarrow{PGM} & \frac{dp}{dz} = -\frac{p}{RT} g \end{cases}$$

DIII

- Vacuum (practical limit is about 10⁻⁸ Pa)
 - Pressure sensors: U-tube, Bourdon tube, diaphragm, piezoelectric...

Questions

(Only one answer is correct)

1. The mass of air in a 30 litre vessel at 27 °C and a gauge pressure of 187 kPa is about?

- a) 1 g
- b) 10 g
- c) 100 g
- d) 1000 g..

2. When a gas in a 30 litre rigid vessel is heated from 50 °C to 100 °C, the pressure ratio: (final/initial):

- a) Doubles
- b) Is closer to 1 than to 2.
- c) Depends on initial volume
- d) Depends on heating speed

3. Liquids:

- a) Cannot be compressed
- b) Cannot be heated by compression
- c) Heat a little bit when compressed, but volume remains the same
- d) Heat up and shrink when compressed

4. The critical temperature of any gas is:

- a) The temperature below which the gas cannot exist as a liquid
- b) -273.16 °C
- c) The temperature above which the gas cannot be liquefied
- d) The temperature at which solid, liquid, and gas coexist

5. In a refrigerator, the amount of heat extracted from the cold side:

- a) Cannot be larger than the work consumed
- b) Cannot be larger than the heat rejected to the hot side
- c) Is inversely proportional to the temperature of the cold side
- d) Is proportional to the temperature of the cold side.



Questions

(Only one answer is correct)

6. Which of the following assertions is correct?

- a) Heat is proportional to temperature
- b) Heat is a body's thermal energy
- c) Net heat is converted to net work in a heat engine
- d) The algebraic sum of received heats in an interaction of two bodies must be null

7. The variation of entropy in a gas when it is compressed in a reversible way is:

- a) Less than zero
- b) Equal to zero
- c) Greater than zero
- d) It depends on the process.

8. The volumetric coefficient of thermal expansion:

- a) Is always positive
- b) Is dimensionless
- c) Is different in the Kelvin and Celsius temperature scales
- d) Is three times the linear coefficient value.
- 9. It is not possible to boil an egg in the Everest because:
 - a) The air is too cold to boil water
 - b) Air pressure is too low for stoves to burn
 - c) Boiling water is not hot enough
 - d) Water cannot be boiled at high altitudes.

10. When a combustion takes place inside a rigid and adiabatic vessel:

- a) Internal energy increases
- b) Internal energy variation is null
- c) Energy is not conserved
- d) Heat flows out.



Exercises

- 1. A U-tube is made by joining two 1 m vertical glass-tubes of 3 mm bore (6 mm external diameter) with a short tube at the bottom. Water is poured until the liquid fills 600 mm in each column. Then, one end is closed. Find:
 - 1. The change in menisci height due to an ambient pressure change, $(\partial z / \partial p_{amb})$, with application to $\Delta p=1$ kPa.
 - 2. The change in menisci height due to an ambient temperature change, $(\partial z/\partial T_{amb})$, with application to ΔT =5 °C.
- 2. An aluminium block of 54.5 g, heated in boiling water, is put in a calorimeter with 150 cm³ of water at 22 °C, with the thermometer attaining a maximum of 27.5 °C after a while. Find the thermal capacity of aluminium.
- 3. How many ice cubes of 33 g each, at -20 °C, are required to cool 1 litre of tea from 100 °C to 0 °C?
- 4. Carbon dioxide is trapped inside a vertical cylinder 25 cm in diameter by a piston that holds internal pressure at 120 kPa. The plunger is initially 0.5 m from the cylinder bottom, and the gas is at 15 °C. Thence, an electrical heater inside is plugged to 220 V, and the volume increases by 50% after 3 minutes. Neglecting heat losses through all walls, and piston friction, find:
 - 1. The energy balance for the gas and for the heater.
 - 2. The final temperature and work delivered or received by the gas.
- 5. Find the air stagnation temperature on leading edges of an aircraft flying at 2000 km/h in air at -60 °C.



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Thermal engineering

Thermodynamics

-<u>Basic</u> (energy and entropy, state properties, state equations, simple processes, phase changes)

–<u>Applied</u> (mixtures, liquid-vapour equilibrium, air conditioning, thermochemistry, power and cold generation, materials processes)

•Heat transfer

- Thermal conduction (solids...)
- Thermal convection (fluids...)
- Thermal radiation (vacuum...)
- Heat exchangers
- Heat generation (electrical heaters...)
- Thermal control systems
- Combined heat and mass transfer (evaporative cooling, ablation...)



Heat transfer

- What is heat (i.e. heat flow, heat transfer)?
 - First law: heat is non-work energy-transfer through an impermeable surf.

$$Q \equiv \Delta E - W = \Delta E + \int p dV - W_{dis} = \Delta H - \int V dp - W_{dis} = (mc\Delta T)_{\text{PIS,non-dis}}$$

- Second law: heat tends to equilibrate the temperature field.

$$\dot{s}_{gen} = \frac{-\nabla T \cdot \dot{\dot{q}}}{T^2}$$

• What is heat flux (i.e. heat flow rate, heat transfer rate)?

$$\dot{Q} \equiv \frac{dQ}{dt} = mc \frac{dT}{dt} \bigg|_{\text{PSM,non-dis}} \equiv KA\Delta T$$

• <u>Heat transfer</u> is the flow of thermal energy driven by thermal nonequilibrium (i.e. the effect of a non-uniform temperature field), commonly measured as a heat flux (vector field).



Heat transfer modes

• How is heat flux density modelled?

 $\dot{q} \equiv \frac{\dot{Q}}{A} = K\Delta T \begin{cases} \text{conduction} & \vec{\dot{q}} = -k\nabla T \\ \text{convection} & \dot{q} \equiv h\left(T - T_{\infty}\right) \\ \text{radiation} & \dot{q} = \varepsilon \sigma \left(T^4 - T_{\infty}^4\right) \end{cases}$

- The 3 ways to change \dot{Q} . K, A, and ΔT .
- K is thermal conductance coeff. (or heat transfer coeff.), k is conductivity, h is convective coeff., ε is emissivity.
- Field or interface variables?
- Vector or scalar equations?
- Linear or non-linear equations?
- Material or configuration properties?
- Which emissivity? This form only applies to bodies in large enclosures.

Heat conduction

Physical transport mechanism

-Short-range atomic interactions (collision of particles in fluids, or phonon waves in solids), supplemented with free-electron flow in metals.

• Fourier's law (1822)

$$\vec{\dot{q}} = -k\nabla T$$

Heat equation

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$$\frac{dH}{dt}\Big|_{p} = \dot{Q} \rightarrow \int_{V} \rho c \frac{\partial T}{\partial t} dV = -\int_{A} \vec{\dot{q}} \cdot \vec{n} dA + \int_{V} \phi dV = -\int_{V} \nabla \cdot \vec{\dot{q}} dV + \int_{V} \phi dV$$
$$\xrightarrow{V \to 0} \rho c \frac{\partial T}{\partial t} = -\nabla \cdot \vec{\dot{q}} + \phi^{\nabla k = 0} = k \nabla^{2} T + \phi, \quad \text{or} \quad \frac{\partial T}{\partial t} = a \nabla^{2} T + \frac{\phi}{\rho c}$$

-with the initial and boundary conditions particular to each problem.

Thermal conductivity

Table 1. Representative thermal conductivity values

	<i>k</i> [W/(m·K)]	Comments	
Order of magnitude for solids	10^2 (good conductors)	In metals, Lorentz's law (1881), $k/(\sigma T)$ =constant	
	1 (bad conductors)	·	
Aluminium	200	Duralumin has $k=174 \text{ W/(m·K)}$,	
		increasing to $k=188 \text{ W/(m \cdot K)}$ at 500 K.	
Iron and steel	50 (carbon steel)	Increases with temperature.	
	20 (stainless steel)	Decreases with alloying	
Order of magnitude for liquids	1 (inorganic)	Poor conductors (except liquid metals).	
	0.1 (organic)		
Water	0.6	Ice has $k=2.3 \text{ W/(m·K)}$,	
Order of magnitude for gases	10^{-2}	Very poor thermal conductors.	
		KTG predicts $k/(\rho c) \equiv a \equiv D_i \equiv v \approx 10^{-5} \text{ m}^2/\text{s}$	
Air	0.024	Super insulators must be air evacuated.	



Simple heat conduction cases

- One-dimensional steady cases
 - Planar $\dot{Q} = kA \frac{T_1 T_2}{L_{12}}$ - Cylindrical $\dot{Q} = k2\pi L \frac{T_1 - T_2}{\ln \frac{R_2}{R_1}}$ - Spherical $\dot{Q} = k4\pi R_1 R_2 \frac{T_1 - T_2}{R_2 - R_1}$

Composite wall (planar multilayer)

$$\dot{q} = K\Delta T = k_{12} \frac{T_2 - T_1}{L_{12}} = k_{23} \frac{T_3 - T_2}{L_{23}} = \dots = \frac{T_n - T_1}{\sum \frac{L_i}{L_1}} \implies K = \frac{1}{\sum \frac{L_i}{L_1}}$$

 \mathbf{I}_{k_i}

Unsteady case. Relaxation time:

 $\Delta t = mc$

$$\Delta T / \dot{Q} \begin{cases} \Delta t \stackrel{Bi >>1}{=} \frac{\rho c L^2}{k} \\ \Delta t \stackrel{Bi <<1}{=} \frac{\rho c V}{hA} \end{cases} \quad Bi = \frac{hL}{k_{\rm S}} \end{cases}$$

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 K_{\cdot}

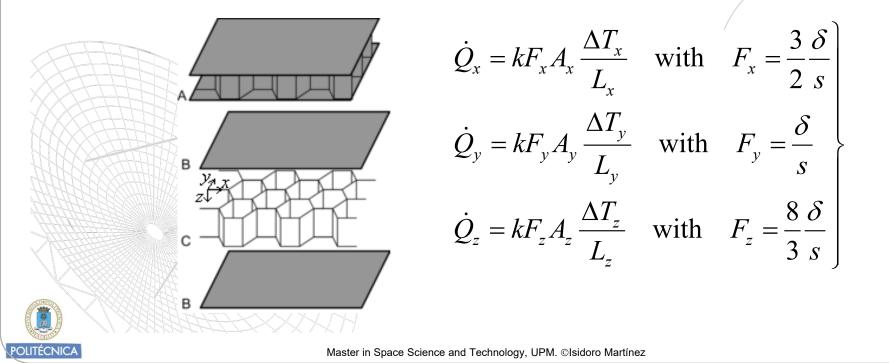
Multiple path in heat conduction

Multidimensional analysis

- Analytical, e.g. separation of variables, conduction shape factors,
- Numerical, finite differences, lumped network, finite elements

Parallel thermal resistances

– Example: honeycomb panel made of ribbon (thickness δ), cell size s:

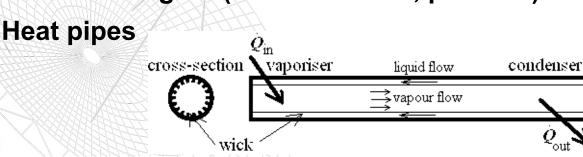


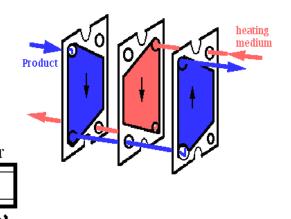
Heat convection

Newton's law and physical mechanism

$$\dot{q} \equiv h \left(T - T_{\infty} \right) = -k \nabla_n T \quad \rightarrow \quad h \Delta T \approx k \frac{\Delta T}{\delta} \quad \rightarrow \quad N u \equiv \frac{hL}{k} = f \left(Re, Pr... \right)$$

- e.g. in air flow, $h=a+bv_{wind}$, with a=3 W/(m²·K) and b=3 J/(m³·K)
- e.g. plate (<1 m)at rest, $h=a(T-T_{\infty})^{1/4}$, with $a\sim 2$ W/(m²·K^{5/4}) (1,6 upper, 0.8 lower, 1.8 vert.)
- Classification of heat convection problems
 - By time change: steady, unsteady (e.g. onset of convection)
 - By flow origin: forced (flow), natural (thermal, solutal...)
 - By flow regime: laminar, turbulent
 - By flow topology: internal flow, external flow
 - By flow phase: single-phase or multi-phase flow
 - Heat exchangers (tube-and-shell, plates...)







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Heat radiation

Heat radiation (thermal radiation)

 It is the transfer of internal thermal energy to electromagnetic field energy, or viceversa, modelled from the basic black-body theory. Electromagnetic radiation is emitted as a result of the motion of electric charges in atoms and molecules.

Blackbody radiation

- Radiation within a vacuum cavity
 - Radiation temperature (equilibrium with matter)
 - Photon gas (wave-particle duality, carriers with zero rest mass, $E=h_V$, p=E/c)
 - Isotropic, unpolarised, incoherent spatial distribution
 - Spectral distribution of photon energies at equilibrium (*E*=const., S=max.)
- Radiation escaping from a hole in a cavity
 - Blackbody emmision

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$$= \frac{2\pi hc^2}{\lambda^5 \left[\exp\left(\frac{hc}{k\lambda T}\right) - 1 \right]} \begin{cases} M = \int_0^\infty M_\lambda d\lambda = \sigma T^4 \quad \sigma = 5.67 \cdot 10^{-8} \frac{W}{m^2 \cdot K^4} \\ \lambda \Big|_{M_\lambda = \max} = \frac{C}{T} \qquad C = 0.003 \text{ m} \cdot K \end{cases}$$



Thermo-optical properties

Propagation through real media

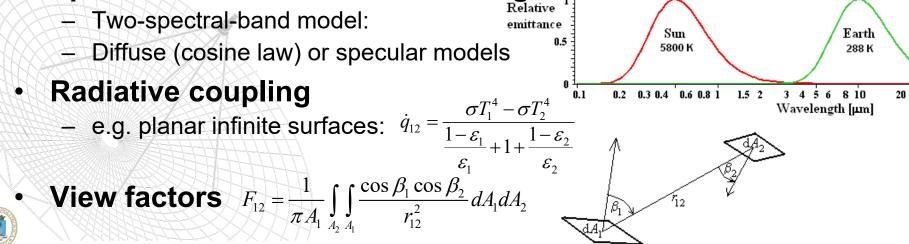
- Attenuation by absorption and scattering (Rayleigh if $d << \lambda$, Mie if $d \ge \lambda$)

Properties of real surfaces

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- Partial absorption (α), reflectance (ρ), emissivity (ε), and, in some cases, transmittance (τ). Energy balance: $\alpha + \rho + \tau = 1$.
- Directional and spectral effects (e.g. retroreflective surfaces, selective glasses...)
- Detailed equilibrium: Kirchhoff's law (1859), $\alpha_{\lambda\beta\thetaT} = \epsilon_{\lambda\beta\thetaT}$, but usually $\alpha \neq \epsilon$

Spectral and directional modelling



Heat transfer goals

Analysis

-Find the heat flux for a given set-up and *temperature* field

e.g.
$$\dot{Q} = kA(T_1 - T_2)/L$$

-Find the temperature corresponding to a given heat flux and set-up

e.g. $T_1 = T_2 + \dot{Q}L/(kA)$

Design

–Find an appropriate material that allows a prescribed heat flux with a given T-field in a given geometry

e.g. $k = \dot{Q}L/(A\Delta T)$

-Find the thickness of insulation to achieve a certain heat flux with a given *T*-field in a prescribed geometry

e.g. $L = kA(T_1 - T_2)/\dot{Q}$

Control

-To prevent high temperatures, use insulation and radiation shields, or use heat sinks and coolers.

-To prevent low temperatures, use insulation and radiation shields, or use heaters.

-To soften transients, increase thermal inertia (higher thermal capacity, phase change materials).



Application to electronics cooling

- All active electrical devices at steady state must evacuate the energy dissipated by Joule effect (i.e. need of <u>heat sinks</u>).
- Most electronics failures are due to overheating (e.g. for germanium at *T*>100 °C, for silicon at *T*>125 °C).
- At any working temperature there is always some dopant diffusion at junctions and bond-material creeping, causing random electrical failures, with an event-rate doubling every 10 °C of temperature increase. Need of <u>thermal control</u>.
- Computing power is limited by the difficulty to evacuate the energy dissipation (a Pentium 4 CPU at 2 GHz in 0.18 μm technology must dissipate 76 W in an environment at 40 °C without surpassing 75 °C at the case, 125 °C at junctions).
- Modern electronic equipment, being powerfull and of small size, usually require liquid cooling (e.g. heat pipes).



Thermal modelling

- Modelling the geometry
- Modelling the material properties
- Modelling the transients
- Modelling the heat equation
- Mathematical solution of the model
 - Analytical solutions
 - Numerical solutions
- Analysis of the results
- Verification planning (analytical checks and testing)
 - Feedback

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Questions

(Only one answer is correct)

1. The steady temperature profile in heat transfer along a compound wall:

- a) Has discontinuities
- b) Must have inflexion points
- c) Must be monotonously increasing or decreasing
- d) Must have a continuous derivative.

2. If the temperature at the hot side of a wall is doubled:

- a) Heat flow through the wall doubles
- b) Heat flow through the wall increases by a factor of 4
- c) Heat flow through the wall increases by a factor of 8
- d) None of the above.

3. When a piece of material is exposed to the sun, its temperature rises until:

- a) It loses and gains heat at the same rate
- b) The heat absorbed equals its thermal capacity
- c) It reflects all the energy that strikes it
- d) No more heat is absorbed.

4. A certain blackbody at 100 °C radiates 100 W. How much radiates at 200 °C?

- a) 200 W
- b) 400 W
- c) 800 W
- d) None of the above.

5. When two spheres, with same properties except for their radius, are exposed to the Sun and empty space:

- a) The larger one gets hotter
- b) The larger one gets colder
- c) The larger one gets hotter or cooler depending on their emissivity-to-absorptance ratio
- d) None of the above.

Exercises

- 1. A small frustrum cone 5 cm long, made of copper, connects two metallic plates, one at 300 K in contact with the smallest face, which is 1 cm in diameter, and the other at 400 K, at the other face, which is 3 cm in diameter. Assuming steady state, quasi-one-dimensional flow, and no lateral losses, find:
 - The temperature profile along the axis.
 - The heat flow rate.
- 2. An electronics board $100 \cdot 150 \cdot 1 \text{ mm}^3$ in size, made of glass fibre laminated with epoxy, and having *k*=0.25 W/(m·K), must dissipate 5 W from its components, which are assumed uniformly distributed. The board is connected at the largest edges to high conducting supports held at 30 °C. Find:
 - 1. The maximum temperature along the board, if only heat conduction at the edges is accounted for (no convection or radiation losses).
 - 2. The thickness of a one-side copper layer (bonded to the glass-fibre board) required for the maximum temperature to be below 40 °C above that of the supports.
 - 3. The transient temperature field, with and without a convective coefficient of h=2 W/(m²·K).
- 3. Find the required area for a vertical plate at 65 °C to communicate 1 kW to ambient air at 15 °C.
- 4. Consider two infinite parallel plates, one at 1000 °C with ε =0.8 and the other at 100 °C with ε =0.7. Find:
 - The heat flux exchanged.
 - The effect of interposing a thin blackbody plate in between.
- 5. Find the steady temperature at 1 AU, for an isothermal blackbody exposed to solar and microwave background radiation, for the following geometries: planar one-side surface (i.e. rear insulated), plate, cylinder, sphere, and cube.



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