



DYNAMIC RESPONSE OF A LIQUID BRIDGE TO AN ACCELERATION VARYING SINUSOIDALLY WITH TIME

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ABSTRACT

The response of a long cylindrical liquid column subjected to an axial microgravity field has been experimentally studied on a TEXUS sounding rocket flight to check with theoretical predictions. The expected response of the liquid bridge was a quasi-static amphora-type deformation of the cylindrical shape. However, the experimental results showed a more complex behaviour. Nevertheless it has been possible to find out the reasons of this discrepancy except for a mysterious 0.5% uncertainty in the stimuli (.

INTRODUCTION

This experiment belongs to a series (SL-1, TEXUS-12, SL-D1, TEXUS-29, SL-D2) on the mechanics of long liquid columns [1]. The proposal was submitted (Feb-91) after conflicting results were obtained from a related Spacelab-D1 (Nov-85) analysis, aiming to elucidate the precise response to an axial acceleration in a presence of g-jitters, before the experiments on Spacelab-D2 (Apr-93), although delays on TEXUS shifted it back to Nov-94.

The nominal configuration is a cylindrical liquid column of radius $R(z)=R_0$ and length L , anchored at the sharp edges of two coaxial solid discs (of radii R_0), held in ambient air by the interface tension σ . This configuration can only be studied in weightlessness. A silicone-oil column of $R_0=15$ mm, $L=85$ mm, $\sigma=0.02$ N/m, density $\rho=920$ kg/m³ and viscosity $\nu=10 \cdot 10^{-6}$ m²/s is used. The shape should be a perfect cylinder at equilibrium if no forces were applied. But the residual microgravity or g-jitters of the carrying platform (SL or TEXUS) is always present, and not very well known, introducing some uncertainty in the comparison with theoretical predictions. Besides, space experiments are so rare that one tries to explore many parameters (bridge stretching, vibration, rotation, eccentric rotation, and so on without having time to make redundancy tests, small variations around a working set-point of parameters, and so on.

During SL-D1, one such a liquid column was undergoing shape oscillations in an amphora-type axisymmetric deformation, with an eigenfrequency and a damping as predicted by theory, but with a deformed mid-shape (averaged over the eigenperiod) corresponding to a theoretical acceleration of $(70 \pm 10) \cdot 10^{-5}$ m/s² (70 ± 10 μ g) constantly acting along the column axis. This high value could not be attributed to the Shuttle drag (< 1 μ g) and remains unexplained. A similar experiment was carried out in SL-D2, but then, applying the same analysis, only a value of 5 ± 1 μ g was found from the averaged deformation of the liquid column.

SCIENTIFIC OBJECTIVES

The main goal of this experiment was to provide a calibrated microgravity acceleration ($100 \pm 1 \mu g$), well above the uncontrolled g -jitters of the platform ($< 1 \mu g$), to check the static response of the liquid column acting as an accelerometer (microgravity accelerometry in the 10^{-3} Hz- 10^{-1} Hz range is still controversial). As a constant controlled acceleration μg -platform is not available, a low varying sinusoidal motion was foreseen.

The acceleration was imposed by a slow sinusoidal translation of the liquid column cell (already used in previous TEXUS flights) along the common column-rocket axes. From the knowledge of the first natural period of the column (15 s) and optimisation of the microgravity time (6 minutes), a forcing period of $T=45$ s was chosen, and a corresponding amplitude of 100 mm peak-to-peak, in order to reach the acceleration quoted above. Six such cycles were allowed during the 5 minutes time available after the formation of the liquid column in orbit, although the first two were expected to be distorted by the initial transients (the half-damping time was known to be some 40 s). Lately, the analysis of Spacelab-D2 results prompted us to leave a full 1 minute to study the decay of the oscillations before re-entry and thus the forcing was reduced to 5 cycles, as shown in Fig. 1. Observe that oscillations start without velocity jump but with a $100 \mu g$ acceleration jump. Nominal displacement law was $z(t)=z_m(1-\cos(2\pi t/T))$, with $z_m=50$ mm and $T=45$ s.

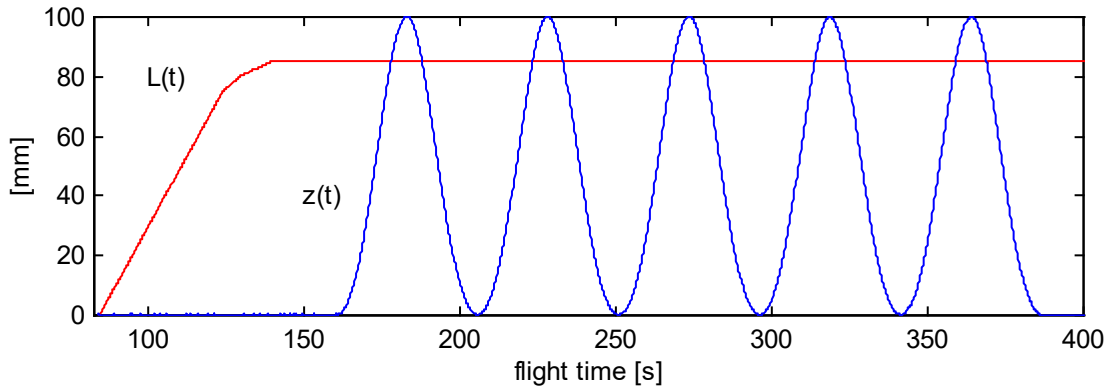


Fig. 1. Disc separation to form the bridge $L(t)$, and cell oscillations $z(t)$ in the experiment.

The expected response of the liquid column was a quasi-static amphora-type deformation of the cylindrical shape, best quantified by the radial deformation in a cross-section at $1/4$ of the column length ($R_{1/4}$), as depicted in Fig. 2.

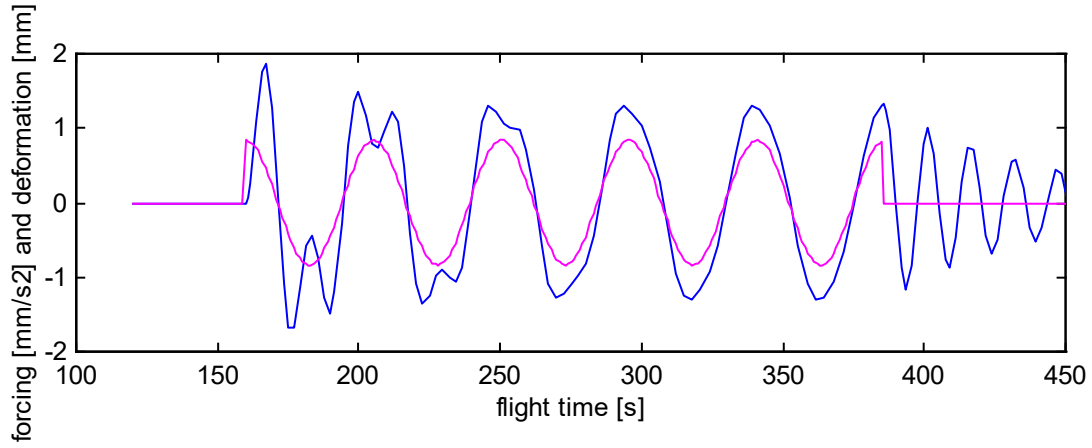


Fig. 2. Ideal excitation (the 5 perfect cycles of the forcing acceleration) and theoretical response of the liquid ($R_{1/4}$ deformation, with damping). After the transients and before the stopping there is a quasi-static amplification in phase.

Consider an initially cylindrical liquid column subjected to an axial acceleration that we name g to resemble gravity, although it is orders of magnitude smaller. The equation governing the equilibrium shape is the Young-Laplace non-linear second-order differential equation of capillary pressure (that accommodates the linear pressure profile inside the liquid to the constant value outside):

$$\sigma \left(\frac{1}{R} + \frac{R_{zz}}{R^2} \right) = \frac{1}{R} p_0 + \rho g z \quad \text{with } R(0) = R(L) = R_0 \quad \text{and} \quad \int_0^L R^2 dz = \pi R_0^2 L \quad (1)$$

which can be numerically solved [2] for the parameters of this problem (R_0, L, ρ, σ) to find first a linear deformation for small g and then a limiting value of g beyond which the bridge breaks. The pressure jump at the origin, p_0 , is an internal constant to be found from the three boundary conditions of the second order problem. In terms of the Bond number, Bo , numerical solving (1) yields $R_{1/4}/R_0 = 1 + 7.8Bo$ and $R_{1/4}/R_0|_{\text{limit}} = 1.19$ (for $Bo = Bo_{\text{limit}} = 0.018$). The linearised analytical solution is:

$$\frac{R_{1/4}}{R_0} = 1 + \frac{L}{4R_0} \left(1 - \frac{1}{\cos \frac{L}{4R_0}} \right) Bo = 1 + \frac{\rho R_0 L}{4\sigma} \left(1 - \frac{1}{\cos \frac{L}{4R_0}} \right) g \quad \text{with} \quad Bo = \frac{\rho g R_0^2}{\sigma} \quad (2)$$

This experiment being not the first in the series, a good deal of work was spent not only analysing the nominal configuration but all conceivable possible departures: the influence of an error in the liquid volume injected (from the nominal cylinder), changes in liquid properties, residual spin of the TEXUS rocket (-3 rpm, and a value of 13 rpm would break the column), change in anchoring radii (in case of bad wetting), etc. Even ground simulation by mounting a Plateau tank in a centrifuge was considered, although abandoned for practical difficulties. All the lessons learnt from past experiments were also applied (redundancy of image recording, background grid to aid in image analysis, all information in the image, etc.)

RESULTS

The results obtained were at first sight all right (large amphora-type deformations), but the detailed analysis was striking, as presented in Fig. 3, due to the fact that the sinusoidal motion was actually achieved by a crank-shaft mechanism, what was not realised by the investigators at the ground tests, where only pen-recorder plots were available (the data acquisition system was not operative).

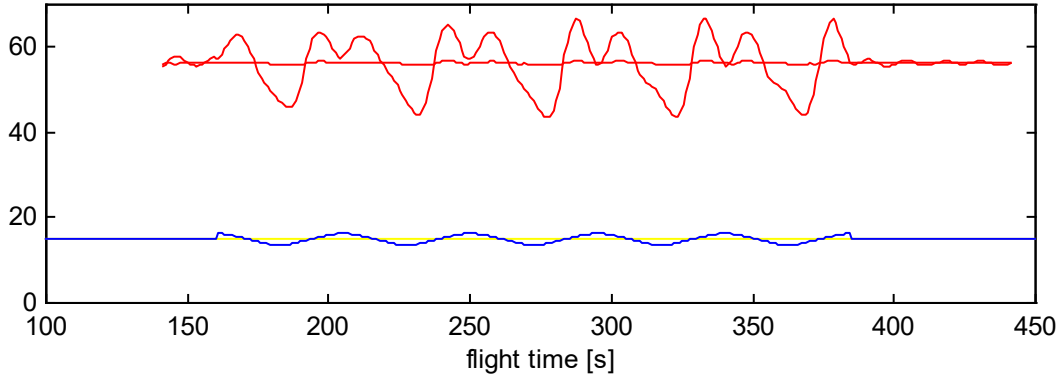


Fig. 3. Discrepancy found in the first analysis of video images. The lower part is the ideal expected $R_{1/4}$ values (and R_0) in mm, and the upper part the real $R_{1/4}$ (and R_0) measurement in pixels.

The analysis of this experiment is based on the recording of cell displacement by a linear potentiometer and the video recording of images of the liquid bridge against a background reference mask and a fixed reference bar to visualise cell displacement. The potentiometer data (used to draw Fig. 1) has a sampling rate of 0.22 s (4.6 Hz) and a resolution of 0.02 mm in 100 mm (12 bit), and from that one infers that the actual column length was $L=85.15\pm0.05$ mm (nominally 85 mm), oscillations started at 160.4 ± 0.1 s flight-time (nominally 160 s) and stopped at 386.6 ± 0.1 s (nominally 385 s), giving a period of 45.2 ± 0.1 s (nominally 45 s), with an amplitude peak-to-peak of 99.8 ± 0.1 mm (nominally 100 mm). The frequency spectrum for the five cycle oscillation is shown in Fig. 4, from two redundant sources, as well as that corresponding to the liquid deformation.

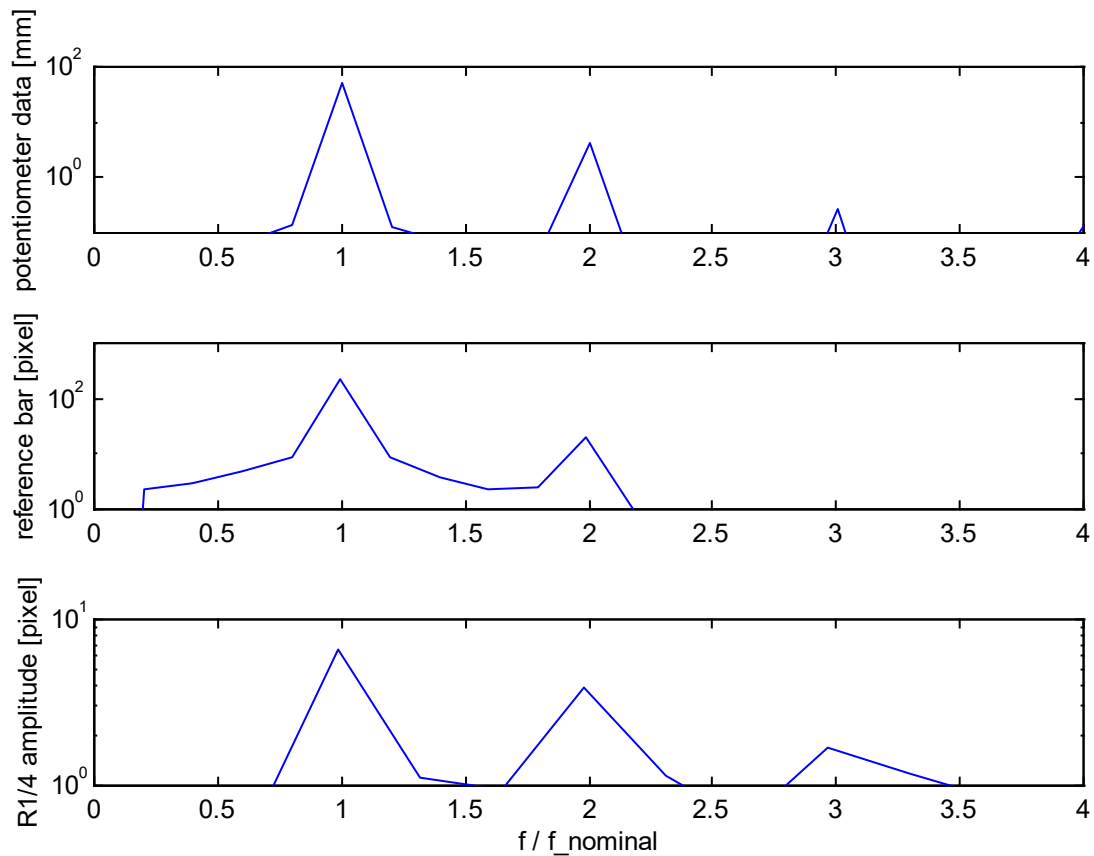


Fig. 4. Fourier analysis of the cell displacement measurement taken by the potentiometer transducer (top), by the reference bar in the image (mid) and of liquid response (deformation at $R_{1/4}$) (bottom).

Taking into account the uncertainty in the potentiometer data one should disregard the fourth harmonic contribution, but the third harmonic remains, with an amplitude of 0.2 ± 0.1 mm still unexplained. From the ratio of the second to the first harmonic, one may deduce the crank shaft length, what yields 158 ± 10 mm (150 mm according to design).

The analysis of the video images is not as straightforward as for the potentiometer data, mainly because of the distortions the analogue video signal suffers before digitization. For instance, for this experiment, an ideal quiescent cylindrical column once processed (CCD, videotape record, videotape playback, digitization) would present a noisy changing shape with uncertainties of 1 pixel in space and 0.5 pixels in time, although if one only considers odd or even videolines (but not both) and liquid column size (i.e. difference in position of the right and left liquid contours) the uncertainty can be reduced to ± 0.2 pixels in the image field, corresponding to ± 0.05 mm in the object field.

The video recording is classified according to the interest for further analysis as follows:

- The 53 s of column formation by liquid injection and disc separation (a small amphora-type deformation is visible, due to the jet injection dynamics).
- The 20 s of calm-down after filling. It turned out to be too short for decay of injection perturbations (the half damping time appears to be $t_{1/2} \approx 35 \pm 5$ s).
- The 90 s of the two first cycles, where transients from the start-up are distorting the periodic response.
- The 135 s of the last three cycles, practically periodic. Fig 5 shows a sequence of frames.

- The 60 s of calm-down after stopping until re-entry. Astonishingly, the deformation after stopping the oscillation is found to be negligible, in contrast to the wide waving expected. A perfect cylinder is seen by the naked eye. No residual acceleration is distinguishable in the finest analysis. Natural period appears to be 13 ± 1 s instead of the expected 15 s, and half-damping time $\approx 35\pm 5$ s instead of 40 s expected.

The axisymmetry, judged by the position and evolution of the centre line (midway between liquid edges at every videoline) is perfect from the beginning up to re-entry of the rocket, where a C-mode deformations grows until breaking the bridge.

The antisymmetry of the liquid shape to the mid-plane between the solid discs is also perfect after the long column is established.

Spectral analysis of the fix-reference bar motion digitised from the video images also shows the second harmonic (and a corresponding crank shaft length of 145 ± 5 mm, but not the third one because a resolution better than one pixel would be needed).

The phase of the crank-shaft mechanism, with the flatten humps in acceleration at the upper part of the cell motion (at start-up and stop-down), is responsible for the dead of the oscillations after stopping the stimulus.

The compound oscillations of the whole TEXUS-rocket, the TEM-06-9 module (fixed to the former by soft mounts), the moving fluid cell and the liquid column itself was analysed: $m_{\text{liquid}}=0.06$ kg, $m_{\text{cell}}=10$ kg, $m_{\text{module}}=60$ kg, $m_{\text{rocket}}=400$ kg. From the μg -accelerometers in the rocket, a train of pulses appear synchronised with our experiment timeline, with pulse amplitude precisely synchronised with the peaks in speed of our cell displacement, and not with acceleration, what might be explained by a series of beating of a loose joint at its bounds.

A one-dimensional dumped-spring model is established to simulate the linear dynamics of the liquid column, once that available liquid bridge theory [3] shows that non-linear effects should be negligible and that the only relevant mode is the first (amphora-type oscillations):

$$\frac{d^2 x(t)}{dt^2} + \frac{2 \ln 2}{t_{1/2}} \frac{dx(t)}{dt} + \left(\frac{2\pi}{T}\right)^2 x(t) = K \left(\frac{2\pi}{T}\right)^2 \ddot{z}(t) \quad (3)$$

where x is the $R_{1/4}$ deformation ($R_{1/4}-R_0$), z the cell displacement, $t_{1/2}=40$ s, $T=15.3$ s and $K=0.24$ deduced from (1) for the static case. The gain in the frequency response of this linear system is shown in Fig.6.

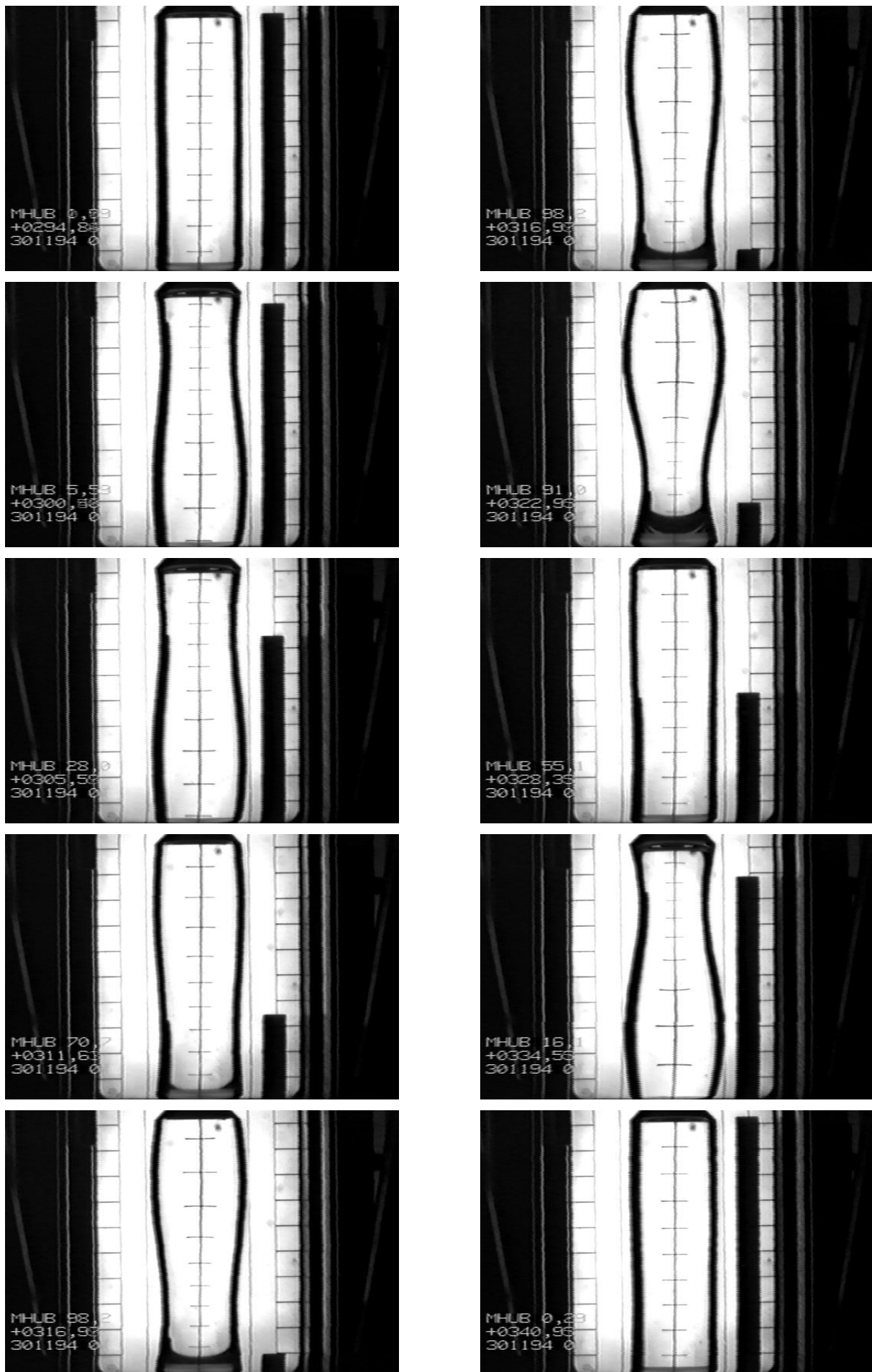


Fig 5. A complete cycle of 45 s in the response of the liquid bridge starting at 294.2 s flight time.

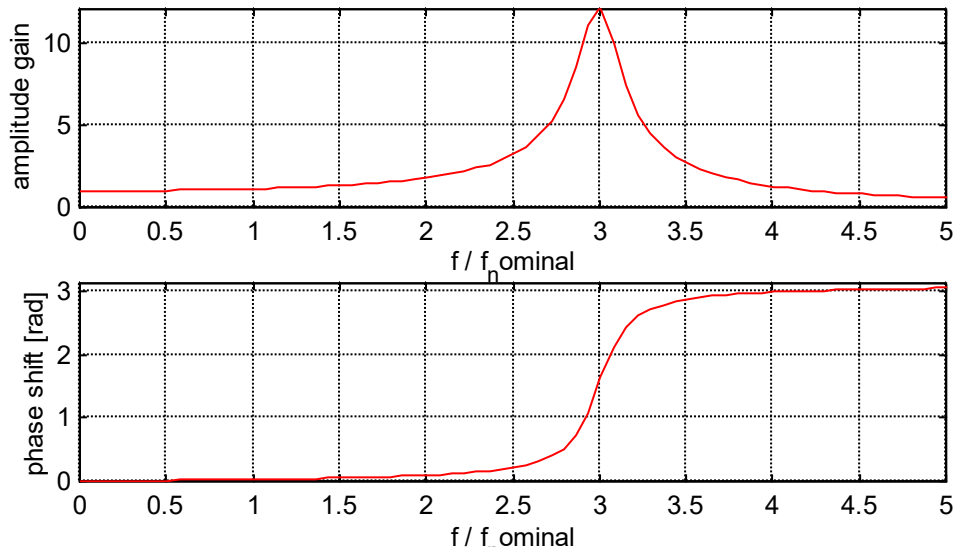


Fig. 6. Frequency response in amplitude and phase of liquid deformation relative to amplitude of stimulus (f_{nominal} corresponds to the $T=45$ s cycling at a third of the eigenfrequency).

Inclusion of the second harmonic from the crank-shaft mechanism explains the camel-shape response in Fig. 3, but there still remains a small third harmonic contribution (some 0.5% of the intended displacement amplitude) that is pervasive to the analysis so far performed. The best matching achieved is shown in Fig. 7

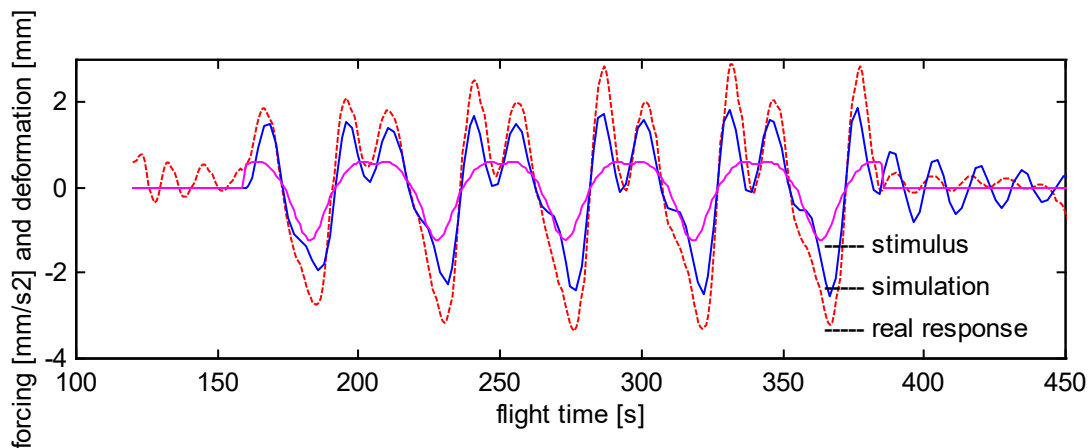


Fig. 7. Real excitation (the humped 5 cycles), real response of the liquid (from video) and expected response (from numerical simulation with (3) and third and fourth harmonics).

CONCLUSIONS

Most aspects of the response of a highly-sensitive long liquid column to a controlled acceleration have been understood in great detail within available theory, and only two puzzling questions remain open:

- an artificial contribution of 0.5% in the applied stimuli to the third harmonic (and maybe of 0.4% to the fourth), is found to better match the real liquid response than the mere crank-shaft motion.
- a phase shift of precisely $\pi/2$ in the acceleration measured in the rocket body and the one applied.

Some lessons have been learnt for future work: 1) even at the high cost of space experiments, time periods to damp-out initial perturbations or to achieved periodic response must be generous, and 2) a negligible 0.5% noise in relative displacement at the eigenfrequency, when driving the system at one third of it, means a

$3^{20.5} = 5\%$ noise in relative acceleration due to the centrifugal effect, and selectively amplified 12 times due to the weak damping, finally yields a $12 \cdot 3^{20.5} = 50\%$ noise in relative response of the liquid bridge.

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1. Martinez, I. Perales, J.M. & Meseguer, J., Stability of long liquid columns, in: Scientific Results of the German Spacelab Mission D2, Sahm, P.R., Jansen, R., Keller, M.H. (Eds.), DFVLR, Köln, FRG, in press, 1995.
2. Perales, J.M., Meseguer, J. & Martinez, I., 1991, Minimum Volume of Axisymmetric Liquid Bridges between Unequal Disks in an Axial Microgravity Field, *Journal of Crystal Growth*, Vol. 110, pp. 855-861.
3. Meseguer, J. & Perales, J.M., 1992, Non-steady Phenomena in the Vibration of Viscous Cylindrical Long Liquid Bridges, *Microgravity Science and Technology*, Vol. 5, pp. 69-72.